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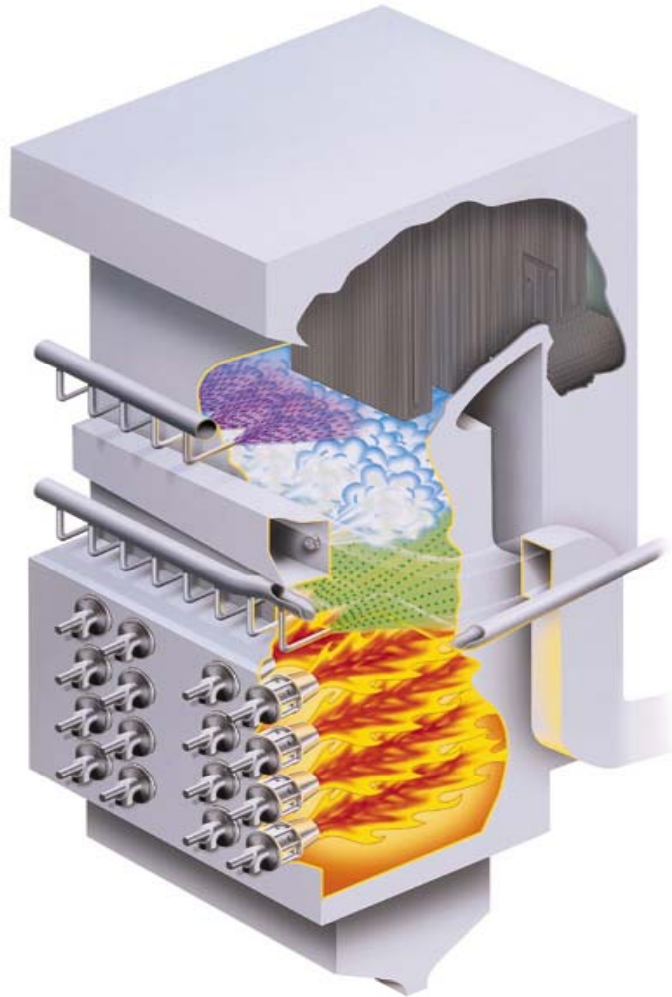


2012 APC Round Table & Expo Presentation

July 16-17, 2012, in Baltimore, MD / Hosted by Duke Energy, Entergy,
FirstEnergy, Southern Company & TVA

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Impact of External Factors on PM Emissions



2012 APC Round Table

Bob Taylor

July 2012

PM Collection – External Factors

- A large part of our daily lives is spent maintaining PM emission limits.
- When emissions approach compliance limits, we are called upon to correct the problem.
- Our first action is generally to review operation of the electrostatic precipitator or fabric filter.
- Aside from maintenance issues, it is likely that the source of the problem may not be the PM control device, but process conditions.
- For this reason, it is critical to consider the whole system when addressing emissions issues.

You have a PM control event

Define the nature of the event to focus your efforts:

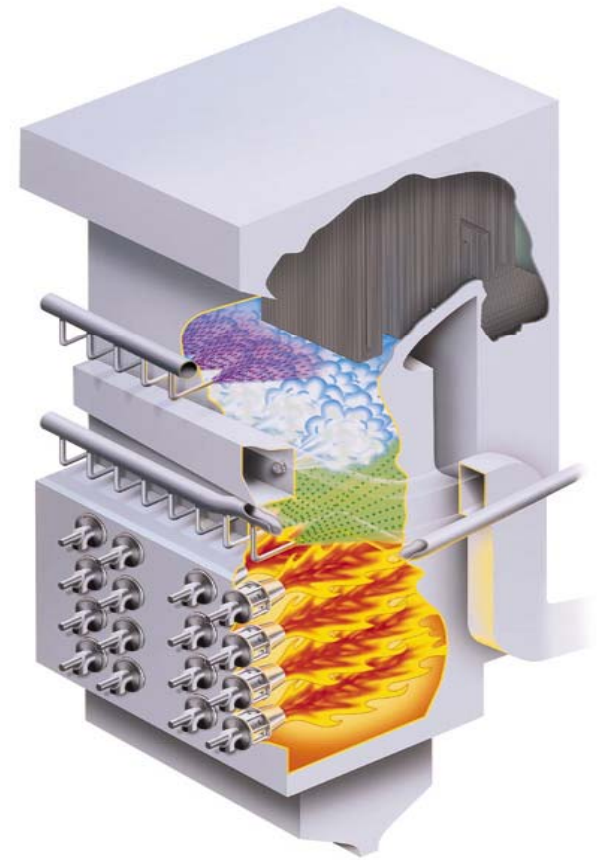
- **Characterize emission levels**
 - Rapid spike
 - Gradual increase
- **Characterize PM event**
 - Random in nature
 - Cyclical based on time or process change
- **ESP - review electrical conditions**
 - Small number of fields affected
 - Consistent impact throughout all fields
- **Fabric filter - review broken bag detector data**
 - High emissions isolated to a single compartment
 - Multiple compartments affected

Where should you look first?

Major factors affecting PM removal:

- Inlet Dust Load
- Flue Gas Flow Rate
- Flue Gas Temperature
- Flue Gas Composition
- Particle Size Distribution
- Carbon Content of Ash
- Introduction of sorbents

Pull historical records to establish baseline



(This will help determine if the problem is the PM control devices fault!)

PM Collection – External Factors

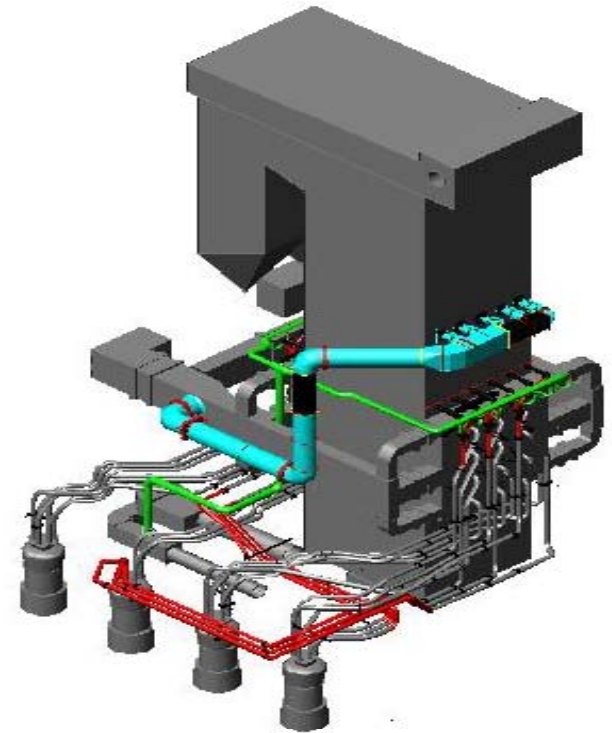
- Most of the fly ash is a constituent of the fuel burned
- As a result, dust loading is proportional to firing rate and ash content of fuel
- Why does inlet dust burden change?
 - Change in load
 - Change in fuel ash content
 - Increased unburned carbon in ash
 - Injection of sorbent ahead of PM device
 - Short term activities such as soot blowing

PM Collection – External Factors

Consider a 250 MW PC boiler burning a Powder River Basin coal:

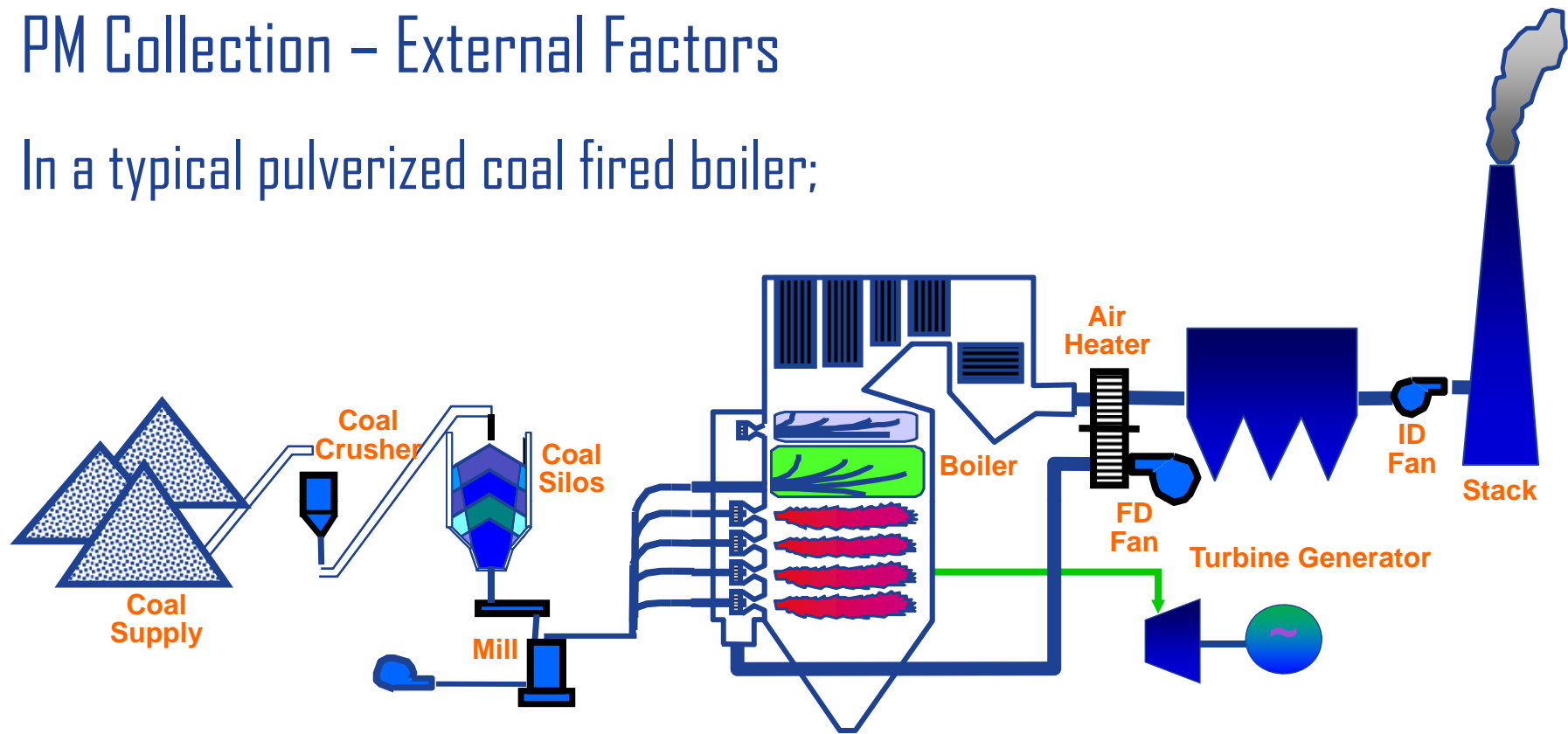
- Coal burn rate: 306,000 lb/hr
- Heating value: 7,850 BTU/lb
- Ash content: 6.5%
- Gas volume: 1,088,000 ACFM
- Gas temperature: 325°F
- Gas pressure: -6" WC
- Dust burden (80%): 6.6 lb/mmBTU

2.87 gr/dscf



PM Collection – External Factors

In a typical pulverized coal fired boiler;



About 15% to 20% of Ash Falls out as Bottom Ash

About 80% to 85% Passes Through Boiler as Fly Ash

For a 250 MW Plant – 9.5 to 10.0 Tons/hr ash

7.5 to 8 Tons/hr fly ash (80%)

PM Collection – External Factors

Example 250 MW Plant

Coal HHV - 7,850 BTU/lb (from Ultimate Analysis)

Heat input – 2,400 mmBTU/hr (Boiler rating)

Fuel burn rate = $(2,400 \text{ mmBTU/hr}) / (7,850 \text{ BTU/lb} / 1,000,000)$
= 306,000 lb coal /hr or 153 tons coal /hr

Coal Ash Content 6.5%

Ash = $306,000 \text{ lb coal /hr} * .065 \text{ lb ash/lb coal}$
= 19,890 lb ash/hr or 9.95 tons ash/hr

At 80% conversion of ash to fly ash

$= 19,890 \text{ lb ash/hr} * 0.8$

= 16,000 lb fly ash/hr or 8 tons fly ash/hr @ 6.5% ash

= 24,615 lb fly ash/hr or 12.3 ton fly ash/hr @ 10% ash

What happens when dust load increases?

Electrostatic Precipitator

- Increased emissions
- Increased spark rate
- Constant pressure drop
- Need for increased rapping
- Potential for increased erosion
- Reduced hopper evacuation cycles

Fabric Filter

- Constant emissions
- Increased pressure drop
- Need to reduce pulse cleaning interval
- Increased bag wear
- Increased compressed air consumption
- Reduced hopper evacuation cycles

What can I do when dust loading increases?

Electrostatic Precipitator

- Increase hopper evacuation rate
- Reduce inlet field collecting plate rapping interval, increase force
- Monitor second field to quantify impact of first field changes
- If using flue gas conditioning, increase SO₃ injection rate

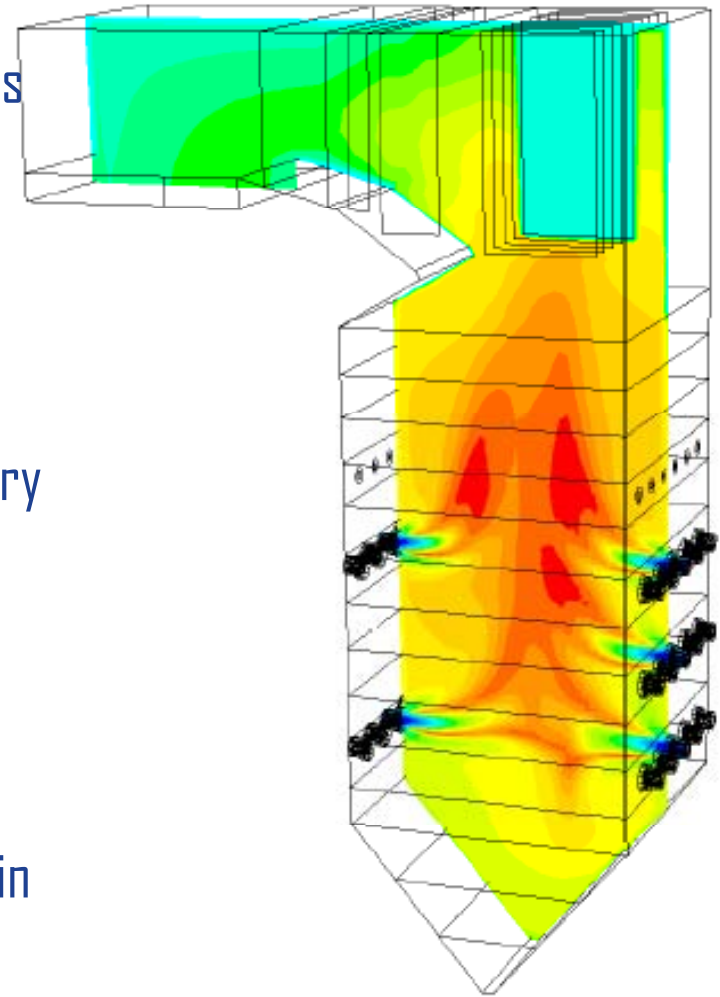
Fabric Filter

- Increase hopper evacuation rate
- If using POD, monitor upper pressure set point limit versus pulsing interval
- If using timer pulsing, decrease interval between pulses
- Monitor sample bags for signs of wear

PM Collection – External Factors

Flue gas Flow Rate

- Flue gas is a combination of combustion products and air in-leakage
- Combustion products are a function of the fuel constituents and the excess air utilized during burning
- Perfect combustion would require a stoichiometry of "1", as defined by fuel composition (Ultimate Analysis)
- Real world, excess is air required since fuel/air mixing less than perfect
- Air in-leakage accounts for significant increase in volume



PM Collection – External Factors

Why does gas volume change?

Factors affecting flue gas volume:

- Fuel burn rate
- Fuel characteristics
- In-leakage
- Moisture content of the gas
- Temperature of the gas

Impact of air in-leakage on Gas Volume

- In a negative pressure PM control device, ambient air will leak into the flue gas
- Consider two O_2 levels in flue gas:
 - 4.5% O_2 $\sim 1,088,000$ ACFM
 - 6.5% O_2 $\sim 1,250,000$ ACFM
- In-leakage causes significant increase in flue gas volume

What impact does this have on PM equipment?

Impact of Gas Volume on ESP

$$EFF = 1 - e^{-\frac{A}{V} w}$$

Increased gas volume
decreases efficiency

$$W = \frac{E_o E_p a}{2 \pi \eta}$$

EFF = Fractional % Collected

A = Surface Area Collecting
Electrodes

V = Volumetric Flow Rate

w = Particle Drift Velocity
or Rate Parameter

E_o = Charging Fields

E_p = Collecting Field

a = Particle Radius

η = Gas Viscosity

π = 3.1416

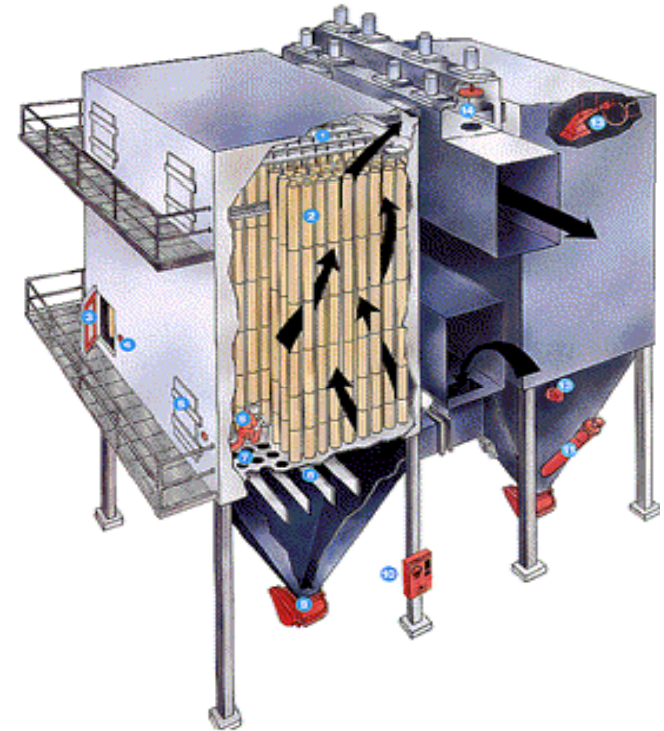
$\frac{\text{Volts}}{\text{Distance}}$

$\frac{\text{Volts}}{\text{Distance}}$

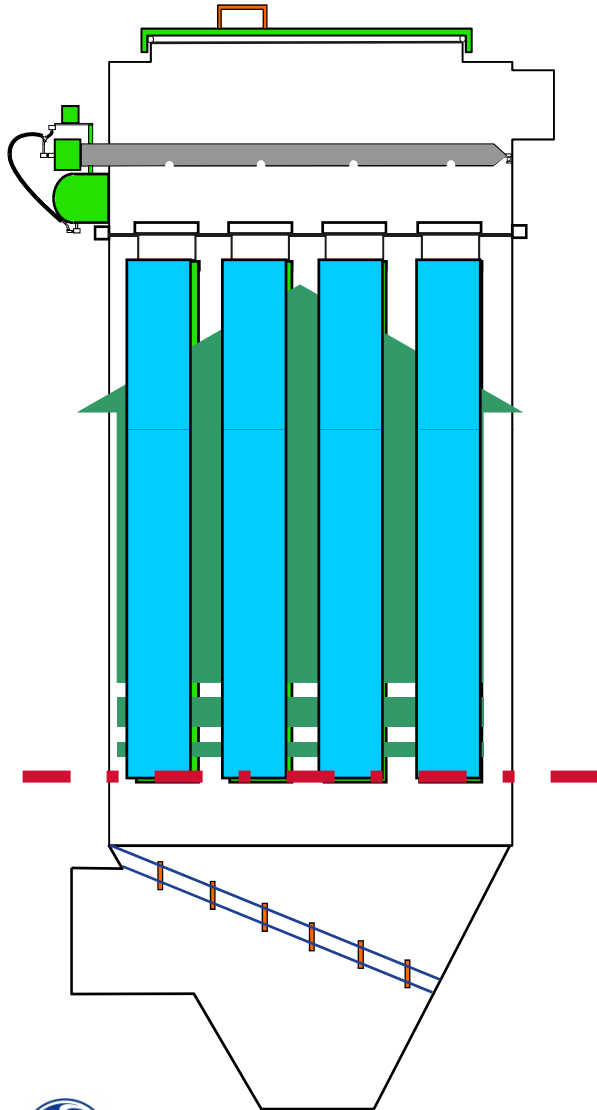
Impact of Gas Volume on Fabric Filter

Air to Cloth Ratio

- Air to cloth ratio = Total gas volume ACFM / Total filter area Ft²
- Filter dia. X length x 3.1415 = Filter area
- Total # Filters x Filter Area = Total Filter Area
- Typical pulse jet air to cloth ratio for utility boilers 2.0 to 4.0 ft/min
 - *Collection efficiency is not volume dependent.*
 - *Increased gas volume results in increased ΔP*



Impact of Gas Volume on Fabric Filter



Can Velocity

In a pulse jet fabric filter, “can” velocity is the upward gas velocity between filter bags.

It is calculated at the horizontal cross section at the bottom of the filter bags.

Excessive can velocity prevents dust from settling into hoppers.

**Increased gas volume results in increased can velocity,
degraded cleaning**

Impact of air in-leakage on Gas Volume

At 2.87 gr/dscf inlet dust loading;

- Impact on ESP
 - 4.5% O₂ ~1,088,000 ACFM
 - 99.4% removal efficiency
 - 0.017 gr/dscf
 - 6.5% O₂ ~1,250,000 ACFM
 - 98.84% removal efficiency
 - 0.033 gr/dscf
- Impact on Fabric Filter
 - 4.5% O₂ ~1,088,000 ACFM
 - 3.5 ft/min Air to cloth ratio
 - 205 ft/min
 - 6.5% O₂ ~1,250,000 ACFM
 - 4.05 ft/min Air to cloth ratio
 - 235 ft/min

ESP emissions almost double

FF pressure drop
~30% increase

Impact of Increased Gas Volume

Electrostatic Precipitator

- Reduced collection efficiency
- Increased pressure drop
- Increased emissions
- Increased abrasion
- Potential hopper sweepage
- Instability in high voltage system

Fabric Filter

- Relatively constant emissions
- Increased pressure drop
- Reduction in cleaning cycle interval
- Reduced bag life
- Inability of dust to settle
- Abrasion from swinging bags and scouring

What should you do when gas volume increases?

Electrostatic Precipitator

- Look for open access points; doors, test ports, poke holes
- Identify and repair chronic sources of in-leakage
- Compare inlet gas temperature to normal conditions
- Minimize outlet field rapping
- Keep hoppers evacuated
- Look for increased spark rate due to HV oscillation

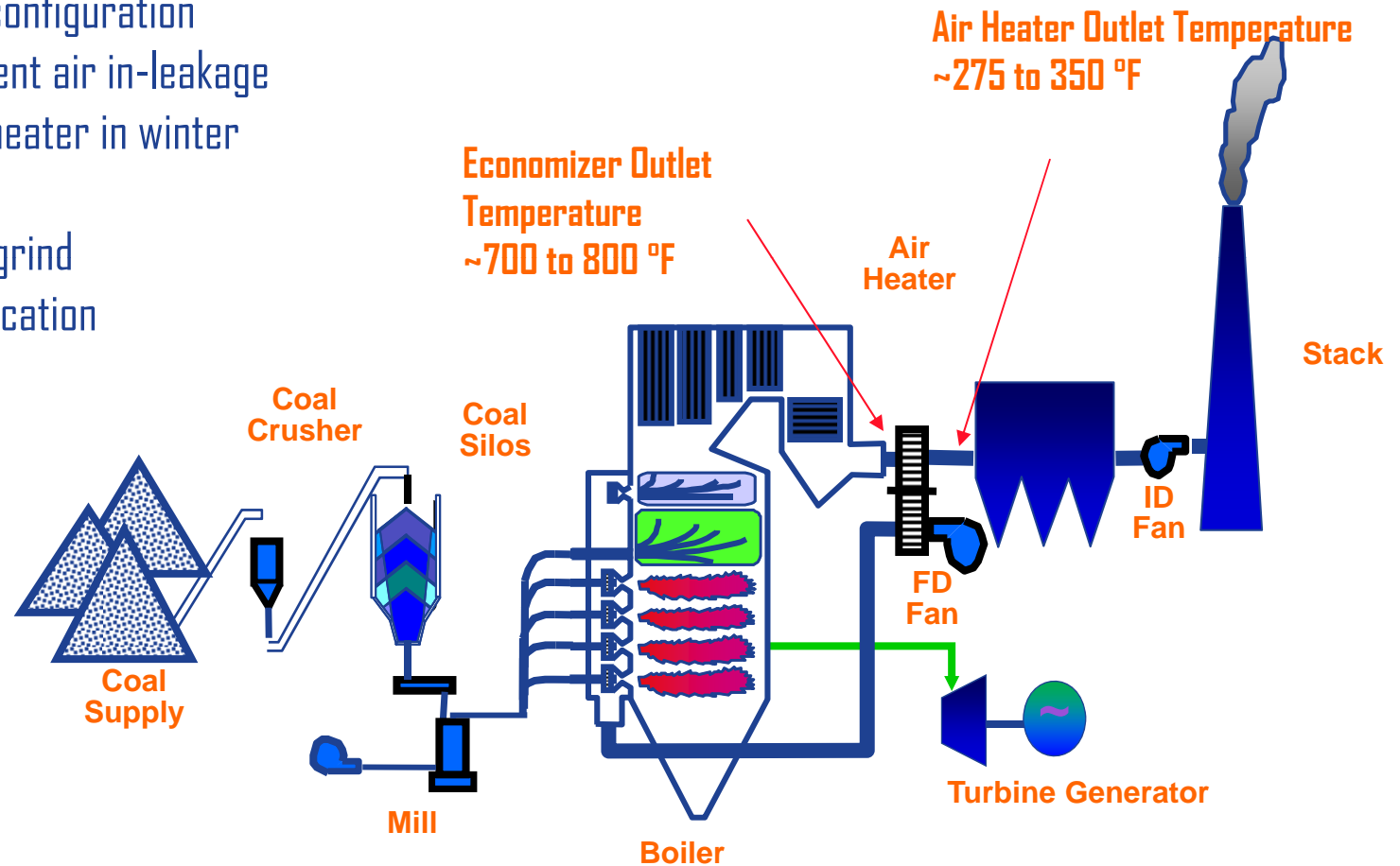
Fabric Filter

- Reduce interval between cleaning cycles, increase upper pressure set point
- Identify and repair sources of in-leakage
- Compare inlet gas temperature to normal conditions
- Bring all compartments on-line
- Obtain sample bags and inspect

Impact of Gas Temperature

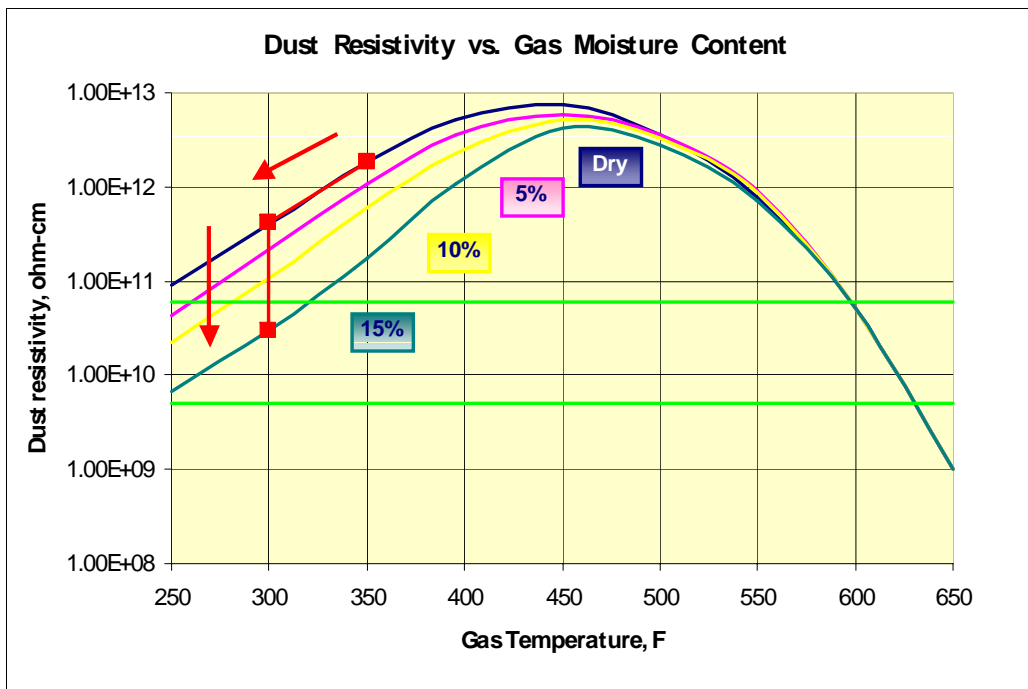
Changes in PM device inlet temperature affects its' operation. Temperature change may result from:

- Slagging or fouling in furnace
- Change in OFA configuration
- Excessive ambient air in-leakage
- Use of air pre-heater in winter
- Load change
- Change in coal grind
- Loss of humidification



Impact of Temperature on PM Collection

- Increasing gas temperature causes dust resistivity to increase on cold side ESP
- This can result in increased ESP's emissions



Estimated emissions:

@1E10 ohm-cm:

0.017 gr/dscf

@7E10 ohm-cm

0.025 gr/dscf

Significant increase in emissions from small change in resistivity

Impact of Temperature on PM Collection

Electrostatic Precipitator

- Increased gas volume
- Possible dust resistivity increase
- Increased emissions
- Damage to insulators
- Damage to elastomer seals
- Reduced sorbent effectiveness
- Possible increase in corrosion.

Fabric Filter

- Increased gas volume
- Reduced fabric life
- Loss of filter bags
- Damage to elastomer seals
- Reduced sorbent effectiveness
- Possible increase in corrosion.

What can I do?

Electrostatic Precipitator

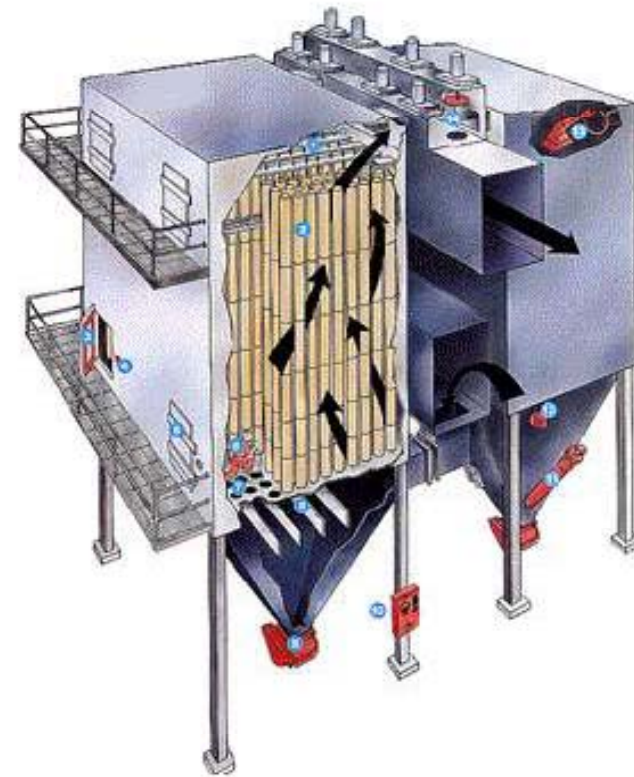
- Monitor secondary current and spark trends.
- If high resistivity;
 - Implement intermittent energization
 - Aggressive collecting plate rapping
 - Reduced power rapping
- Blow soot (Steam)
- If temperature too low, reduce in-leakage
- Consider adding moisture

Fabric Filter

- Monitor temperature relative to media limits.
- If temperature too high, bleed in ambient air or introduce EGC.
- If temperature too low, reduce in-leakage or reduce water injection rate.

Impact of Fuel Composition

- As shown previously, composition of the coal affects dust burden and gas volume
- In addition, gas composition can affect other factors:
 - Sulfur & iron oxide affect acid dew point and resistivity
 - Moisture affects volume, resistivity, and acid dew point
 - Incomplete combustion increases carbon monoxide and carbon content of ash



Fabric Characteristic Chart

Characteristic	Polypropylene	Polyester	Acrylic	Fiberglass ¹	Nomex® (Aramids)	PPS	P84 ^{2,3}	Teflon or other PTFEs ³
Max. continuous operating temperature	170°F (77°C)	275°F (135°C)	265°F (130°C)	500°F (260°C)	400°F (204°C)	375°F (190°C)	450°F (232°C)	500°F (260°C)
Abrasion Resistance	Excellent	Excellent	Good	Fair	Excellent	Good	Fair	Good
Energy Absorption	Good	Excellent	Good	Fair ¹	Good	Good	Good	Good
Filtration Properties	Good	Excellent	Good	Fair	Excellent	Excellent	Excellent	Fair
Moist Heat	Excellent	Poor	Excellent	Excellent	Good	Good	Good	Excellent
Alkalines	Excellent	Fair	Fair	Fair	Good	Excellent	Fair	Excellent
Mineral Acids	Excellent	Fair	Good	Poor ^A	Fair	Excellent	Good	Excellent
Oxygen (>15%)	Excellent	Excellent	Excellent	Excellent	Excellent	Poor	Excellent	Excellent
Relative Cost (1 low-10 high)	1	1	2	3	4	5	6	7
Fabric Finishes								
Non-Fiberglass	Purpose of Finish				Available for			
Single	Improved dust cake release				Polyester, Polypropylene, Acrylic, Nomex®, PPS, P84 (Felts)			
Gloss / Eggshell	Short-term improvements for dust cake release (may impede gas flow)				Polyester, Polypropylene (Felts)			
Silicone	Aids initial dust cake development and provides limited water repellency				Polyester (Felt and woven)			
Flame Retardant	Retards combustibility (Not flame-proof)				Polyester, Polypropylene (Felt and woven)			
Acrylic Coatings (Latex base)	Improved filtration efficiency and cake release (May impede gas flow in certain applications)				Polyester and Acrylic felts			
PTFE Penetrating Finishes	Improved water and oil repellency; limited cake release				Nomex® (Aramid felts)			
BHA-TEX® (PTFE Membrane)	For capture of fine particulate, improved filtration efficiency, cake release, and gas flow capacity.				Nomex®, Polyester, Acrylic, Polypropylene (Felt and woven), P84, PPS, PTFE			
Fiberglass	Purpose of Finish				Applications			
Silicone, Graphite, Teflon	Protects glass yarns from abrasion, adds lubricity				Non-acidic applications, primarily for cement, other rock dust and metal foundry applications			
Acid Resistant	Shield glass yarn from acid attack				Coal-fired boilers, carbon black, incinerators, cement industrial boiler applications			
Teflon B	Provides enhanced fiber to fiber resistance and limited chemical resistance				Industrial and utility base load boilers under mild pH conditions			
Blue Max CRF-70® magination at work	Provides improved acid resistance and reduces fiber to fiber abrasion, resistant to alkaline attack, improved fiber encapsulation				Coal-fired boilers (high and low sulfur) for peak load operating cycle, fluidized bed boilers, carbon black, incinerators			
BHA-TEX® (PTFE Membrane)	For capture of fine particulate, improved filtration efficiency, cake release, and gas flow capacity.				Cement / lime kilns, incinerators, coal-fired boilers, cupola, ferro silica / alloy, furnace			



Impact of Coal Composition

Electrostatic Precipitator

- Increased moisture can benefit dust resistivity.
- Increased acids can benefit dust resistivity
- Excessive moisture or acids can degrade rapping and increase corrosion
- Elevated CO possible explosion

Fabric Filter

- Increased moisture can lead to bag blinding
- Increased acids can degrade fabrics
- Excessive oxygen can degrade some fabrics
- Excessive moisture can degrade some fabrics.
- Elevated CO possible explosion

Response to Coal Composition

Electrostatic Precipitator

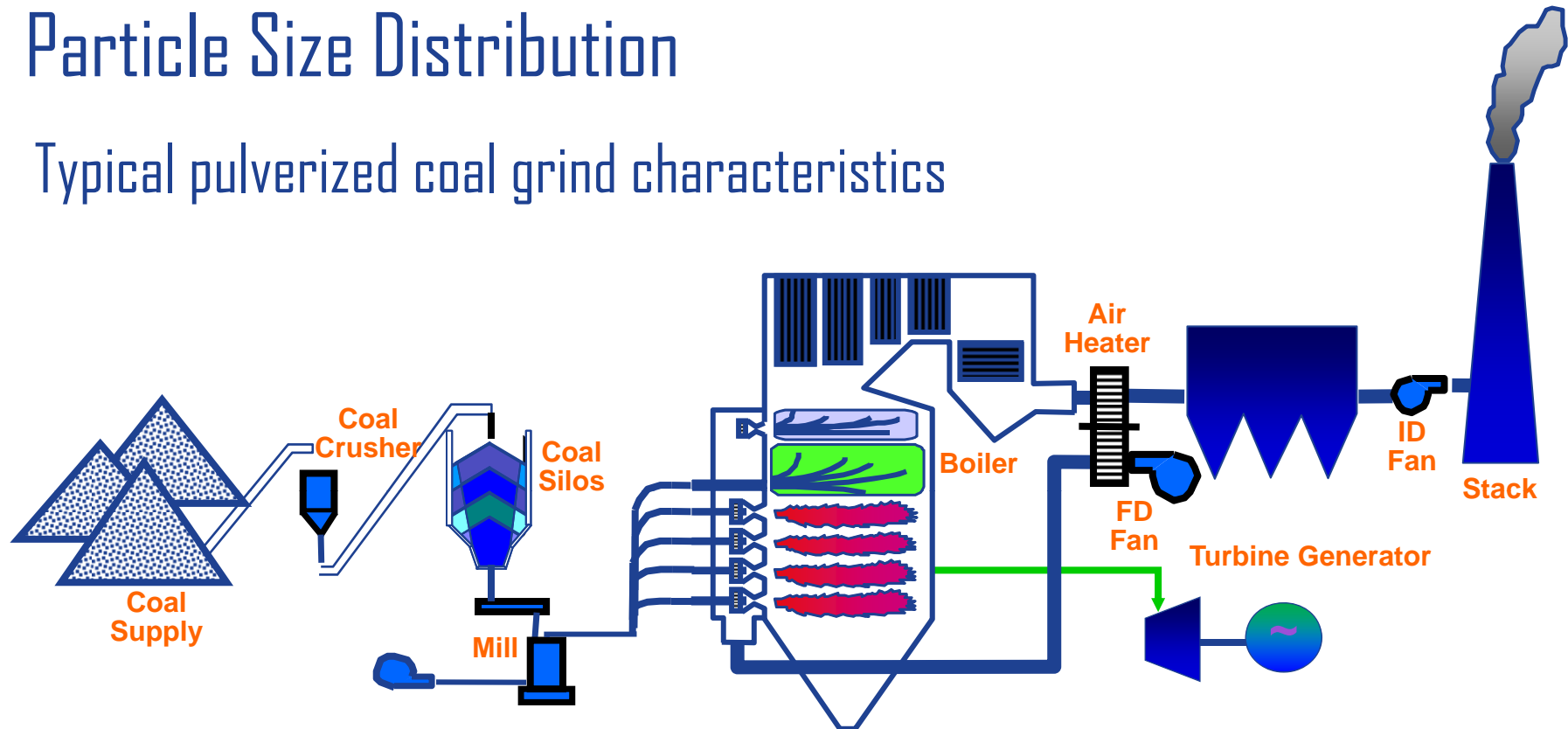
- Monitor dew point of gas stream and adjust inlet temperature
- Adjust rapping intensity and frequency when dust resistivity changes
- Modify FGC system injection rate based on secondary current and spark rates

Fabric Filter

- Increase pulse frequency when moisture make dust sticky
- Monitor change in acids relative to media capabilities
- Improve coal grind to lower excess air
- Inject alkali ahead of FF to react with acids

Particle Size Distribution

Typical pulverized coal grind characteristics



Crusher ~ 1" "particles"

Mills - 70% through 200 mesh screen – 125 microns

Fly ash particle size is a function of coal grind and coal characteristics (volatile content)

Particle Size Distribution

Particle size is partially a function of coal, partially the preparation process:

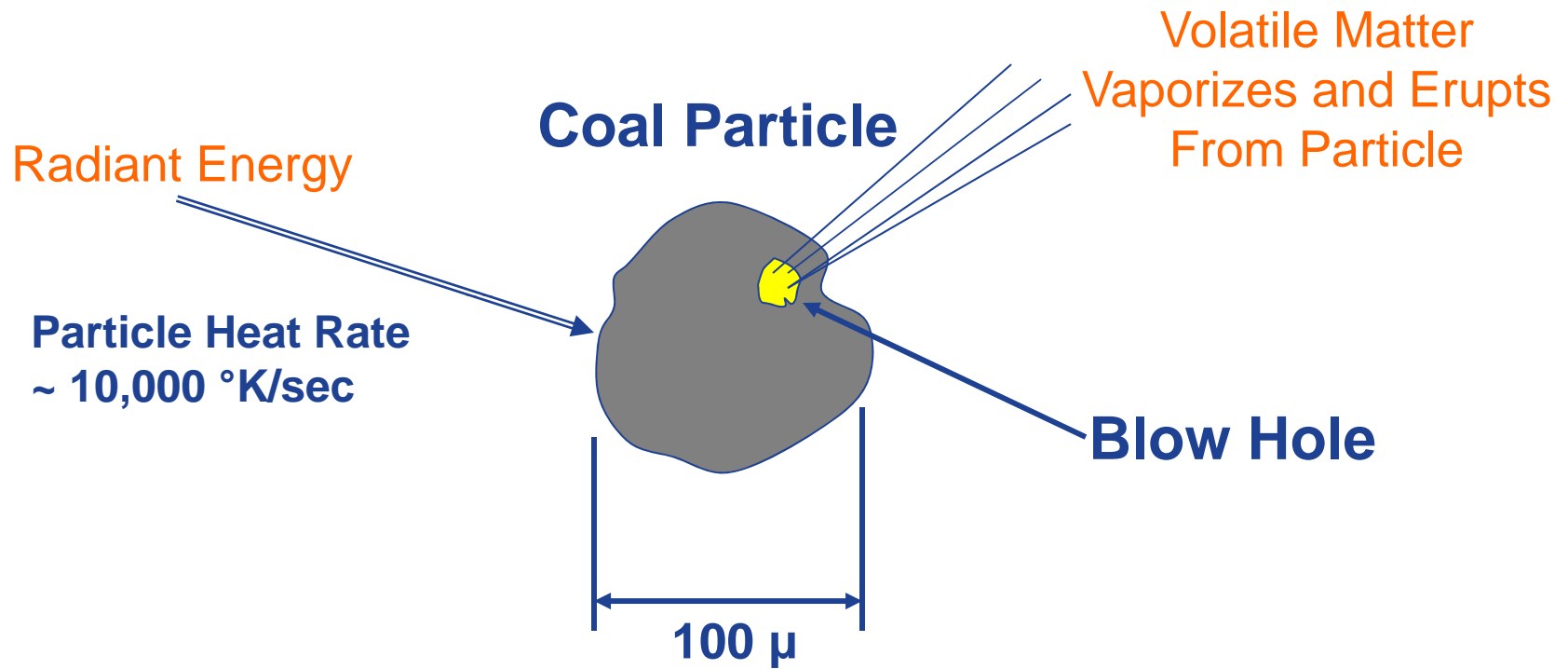
Volatile matter

- Volatile matter burns like a gas flame
- Rapid oxidation but MAY form soot based on local oxygen deficiency
- Increased volatile content associated with **fine dust**

Fixed Carbon

- Often referred to as "Char"
- Burns by surface reaction - oxygen diffusion
- End product is a burned out hulk of inorganic material
- Lattice structure generally broken as they pass through convective sections – **coarse dust**

Impact of Particle Size Distribution



Typical coal combustion of volatile matter

Impact of Particle Size on ESP

$$EFF = 1 - e^{-\frac{A}{V} w}$$

Reduced particle size
decreases efficiency.

$$W = \frac{E_o E_p a}{2 \pi \eta}$$

EFF = Fractional % Collected

A = Surface Area Collecting
Electrodes

V = Volumetric Flow Rate

w = Particle Drift Velocity
or Rate Parameter

E_o = Charging Fields

$\frac{\text{Volts}}{\text{Distance}}$

E_p = Collecting Field

$\frac{\text{Volts}}{\text{Distance}}$

a = Particle Radius

η = Gas Viscosity

π = 3.1416

Impact of Reduced Particle Size

Electrostatic Precipitator

- Reduced collection efficiency
- Excessive space charge conditions; current suppression
- Increased potential for re-entrainment.
- Elevated impact on opacity

Fabric Filter

- Potential bag blinding
- Fabric “bleed Thru”
- Possible increased emissions
- Increased pressure drop due to lack of “settling”
- Elevated impact on opacity

What can I do?

Electrostatic Precipitator

- Improve gas flow uniformity to eliminate channeling
- Monitor spark rates and space charge, HV stability
- Eliminate sneakage or sweepage
- Maximize field strength
- Increase rapper off times to maximize agglomeration
- Consider agglomeration methods

Fabric Filter

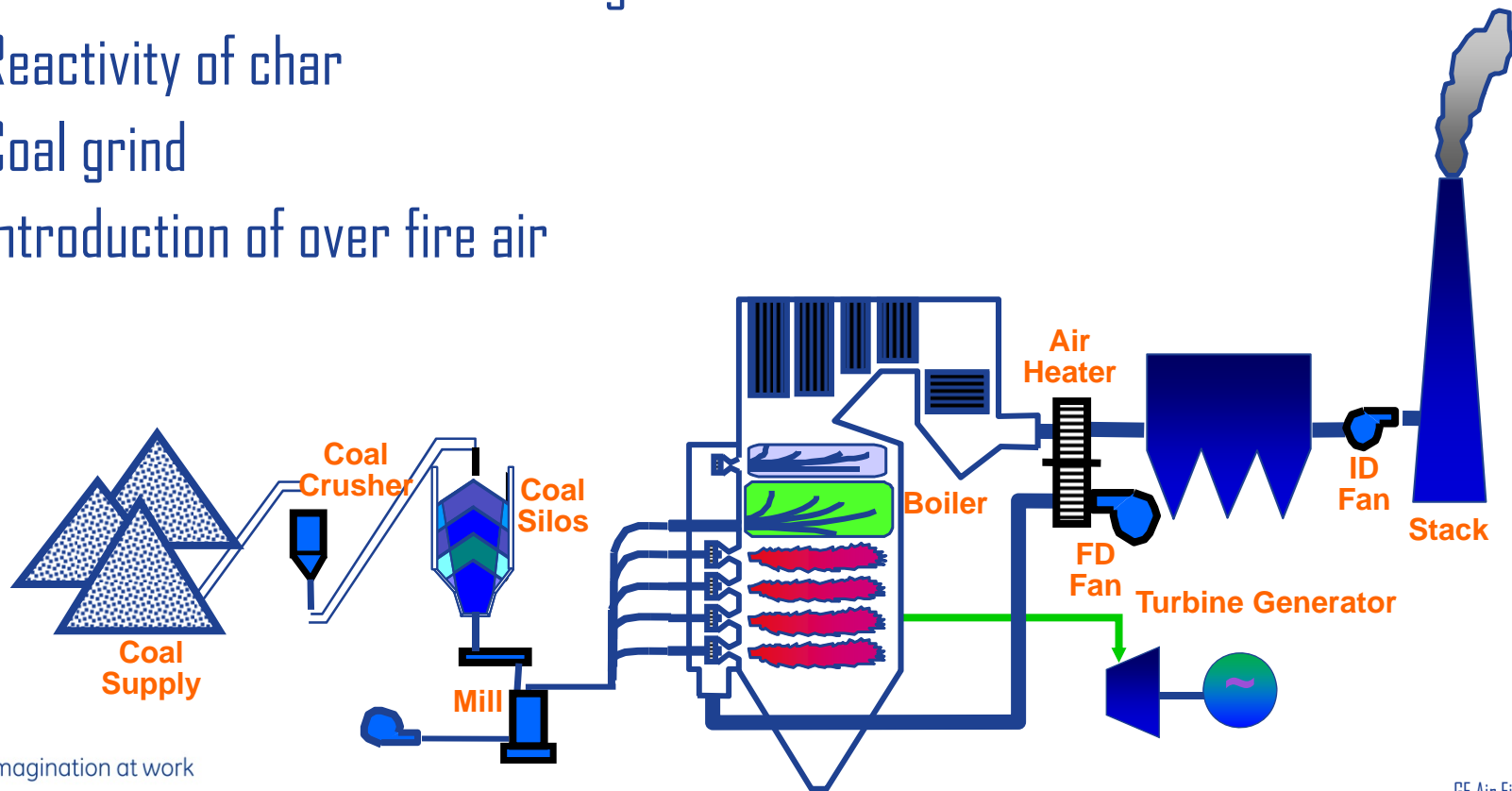
- Pre-coat filter bags
- Change to felt from woven
- Consider membrane laminated filter media
- Decrease pulse pressure and cycles
- Improve internal gas distribution
- Consider agglomeration methods

Carbon in Fly Ash

Incomplete burn out increases unburned carbon in ash

Factors Affecting Complete Burn Out

- Residence time from burners to nose
- Effectiveness of fuel/air mixing
- Reactivity of char
- Coal grind
- Introduction of over fire air



Carbon in Fly Ash

Other Sources of Carbon in Fly Ash

- Incomplete combustion is not the only reason for carbon in ash
- Mercury control strategies utilizing carbon based sorbents are another reason
- Powdered activated carbon is injected into the gas stream ahead of the PM control device
- This process increases the dust burden to the PM control device

Impact of PAC Injection on Dust Burden

Total Dust Burden				
PAC Rate lb/mmBTU	Inlet Dust gr/acf	PAC Injection gr/acf	Total Burden gr/acf	% Increase
1.5	1.5	0.011	1.511	0.73
3	1.5	0.022	1.522	1.50
7	1.5	0.049	1.55	3.33
Polishing Mode				
PAC Rate lb/mmBTU	Inlet Dust gr/acf	PAC Injection gr/acf	Total Burden gr/acf	% Increase
1.5	0.015	0.011	0.026	173.00
3	0.015	0.022	0.037	247.00
7	0.015	0.049	0.064	427.00

Injecting PAC ahead of ESP - minimal impact on FF dust burden

Injecting after ESP - major impact on FF dust burden

Carbon Content of Ash

- An ESP is not as effective at removing carbon as compared to fly ash
- Field testing indicates ESP emissions may increase when PAC is utilized
- Performance is a function of the number of electrical fields, gas velocity, and general condition of ESP
- Carbon has lower reflectance when compared to fly ash (Increased visible emissions)
- Field testing indicates PAC can create potential for hopper fires

Impact of Carbon in Fly Ash

Electrostatic Precipitator

- Increased spark rate
- Increased re-entrainment
- Potential for insulator tracking
- Potential for hopper fires
- Inability to sell fly ash
- Decreased effectiveness of activated carbon
- Potential increased dust resistivity.

Fabric Filter

- Hydrocarbons can blind filter bags
- Potential for hopper fires
- Inability to sell fly ash
- Decreased effectiveness of activated carbon

What can I do?

Electrostatic Precipitator

- Maintain elevated secondary current densities
- Minimize outlet field rapping
- Eliminate hopper in-leakage
- Monitor operation of hopper heating equipment
- Eliminate internal stabilizer insulators
- Pressurize support insulators
- Consider agglomeration
- Evacuate hoppers frequently
- Verify proper coal grind
- Balance primary and over fire air

Fabric Filter

- Pre-coat new filter bags to avoid blinding
- Consider membrane laminated filter media
- Establish “sacrificial” start-up compartment
- Empty hoppers frequently
- Minimize hopper in-leakage
- Monitor operation of hopper heating equipment
- Verify proper coal grind
- Balance primary and over fire air

Summary

- The PM control device may not be the source of emission problems
- Multiple external factors impact operation of the PM control device
- The PM device has no direct influence over these parameters
- Understanding conditions associated with “Normal” operation helps when trouble shooting
- Define process parameters that have most impact on equipment operation and establish trending
- Understand the result of changes in any of the critical parameters
- Do not focus on any single area, the problem is likely a combination of issues